

Multiscale analysis of shear failure of thick-walled hollow cylinder in dry sand

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A novel hierarchical multiscale model has been applied to simulate the thick-walled hollow cylinder tests in dry sand and to investigate the corresponding shear failures. The combined finite-element method and discrete-element method (FEM/DEM) model employs the FEM as a vehicle to advance the solution for a macroscopic non-linear boundary value problem incrementally. It is, meanwhile, free of conventional macroscopic phenomenological constitutive law, which is replaced by discrete-element simulations conducted with representative volume elements (RVEs) associated with the Gauss quadrature points of the FEM mesh. Numerical simulations proposed by the authors indicate that this multiscale approach is capable of replicating the evolution of cavity pressure during cavity expansion – before and after the onset of strain localisation – in qualitative agreement with laboratory tests. In particular, the curvilinear shear bands observed from experiments have been reproduced numerically. The information provided by the mesoscale DEM and the macroscale FEM reveals a close linkage between significant particle rotations taking place inside the dilative shear bands and the highly anisotropic microstructural attributes of the associated RVEs.

KEYWORDS: anisotropy; numerical modelling; strain localisation

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NOTATION

\mathbf{D}_{ijkl}	tangent operator of an RVE packing
\mathbf{d}_i^c	branch vector of two contacting particles
E_c, ν_c	interparticle contact parameters for the DEM model
e	void ratio of an RVE packing
\mathbf{f}_i^c	interparticle contact force
G	macroscopic elastic shear modulus of the RVE
k_n, k_t	normal and tangential contact stiffnesses
N_c	contact number within an RVE packing
$\mathbf{n}_i^c, \mathbf{t}_i^c$	normal and tangential unit vectors at a contact
V	volume of an RVE packing
$\alpha, \beta, \gamma, \delta$	material strength coefficients for calculating the analytical cavity pressure limit
ϵ_1, ϵ_3	major and minor principal strains
θ	average particle rotation of an RVE packing
σ_1, σ_3	major and minor principal stresses
σ_{ij}	effective stress tensor
ϕ	interparticle friction angle for the DEM model
$\phi'_{\max}, \psi_{\max}$	macroscopic peak friction angle and peak dilation angle of the RVE

INTRODUCTION

Cavity expansion in thick-walled hollow cylinder (TWHC) tests is of great importance for practicing geotechnical engineers and researchers (Carter *et al.*, 1986; Mántaras & Schnaid, 2002). In engineering practice, the mechanical response of soil during cavity expansion dictates the resultant CPT number obtained from the cone penetration test and the estimated shear strength of the soil (Salgado

et al., 1997). Cavity expansion may also occur during the pile-driving process in foundation engineering. It is also an important physical process that affects the stability of boreholes (Yu, 2000).

Cavity expansion replicated in TWHC tests also plays an important role for the theoretical study of soil behaviour. It may provide a complementary perspective to the conventional/true triaxial tests for a better understanding of soil behaviours subjected to complex loading paths. In particular, the intriguing failure patterns in TWHC tests have captured the attention of numerical modellers. In the literature, the bifurcation theory has been applied to predict the shear failure of TWHC based on various phenomenological constitutive models (Vardoulakis & Papanastasiou, 1988; Papanastasiou & Vardoulakis, 1989; Anand & Gu, 2000; Sun, 2013). Notwithstanding their success, these models require a large number of internal variables to capture the inherent anisotropy and evolution of fabric (Zervos *et al.*, 2001; Crook *et al.*, 2003; Sun, 2013, 2015). To overcome these pitfalls, a novel multiscale approach (Kaneko *et al.*, 2003; Miehe & Dettmar, 2004; Andrade *et al.*, 2011; Guo, 2014; Guo & Zhao, 2014, 2015; Nguyen *et al.*, 2014; Desrues *et al.*, 2015; Liu *et al.*, 2015b; Zhao & Guo, 2015a, 2015b) is adopted in this study. The adopted approach employs the finite-element method (FEM) to simulate the macroscopic boundary value problem. Meanwhile, it replaces the phenomenological constitutive law needed in conventional FEM with discrete-element method (DEM) computations at the Gauss quadrature points of the FEM mesh. Each Gauss point is associated with a granular assembly in the size of the representative volume element (RVE). At each loading step, the macroscopic deformation of the granular assemblies is prescribed and the macroscopic Cauchy stress updates are inferred from the deformed RVEs for the global FEM computation.

This multiscale approach provides several advantages. First, the path-dependent behaviours obtained from the simulations are directly related to the grain rearrangements that lead to the formation and collapse/buckling of force

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chains and branch vectors (Tordesillas, 2007; O’Sullivan *et al.*, 2013; Sun *et al.*, 2013a). Hence, there is no need to introduce an excess amount of internal variables to curve-fit the phenomenological responses for specific stress path during cavity expansion (Liu *et al.*, 2015a). Furthermore, the coupling of continuum-scale FEM and grain-scale DEM offers a natural pathway to bridge grain-scale mechanics to field applications. Due to the multiscale coupling, the evolution of microstructural attributes under macroscopic external loading can be examined conveniently. These salient features are exploited to replicate numerically the complex failure patterns commonly observed in the TWHC tests in this study.

APPROACH AND FORMULATION

In each macroscopic loading step, DEM simulations are performed at the Gauss quadrature points to provide macroscopic constitutive updates. The macroscopic FEM model is solved implicitly by way of the Newton–Raphson iterative scheme. In each iteration, the deformation at each Gauss point is first interpolated by way of the macroscopic shape function and this is subsequently applied as the local boundary condition for each RVE. After the DEM computation, the updated stress tensor σ_{ij} and the tangent operator \mathbf{D}_{ijkl} can be homogenised using the following equations

$$\sigma_{ij} = \frac{1}{V} \sum_{N_c} \mathbf{d}_i^c \mathbf{f}_j^c \quad (1)$$

$$\mathbf{D}_{ijkl} = \frac{1}{V} \sum_{N_c} \left(k_n \mathbf{n}_i^c \mathbf{d}_j^c \mathbf{n}_k^c \mathbf{d}_l^c + k_t \mathbf{t}_i^c \mathbf{d}_j^c \mathbf{t}_k^c \mathbf{d}_l^c \right) \quad (2)$$

where V is the volume of the RVE packing; N_c is the number of interparticle contacts; \mathbf{d}_i^c is the branch vector; \mathbf{f}_i^c is the contact force; \mathbf{n}_i^c and \mathbf{t}_i^c are the normal and tangential unit vectors at the contact, respectively; and k_n and k_t are the normal and tangential contact stiffnesses, respectively.

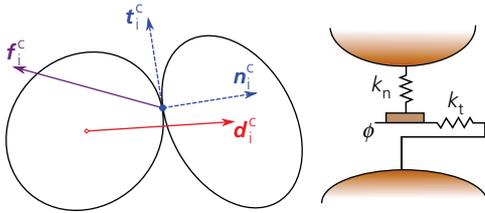


Fig. 1. Illustration of an interparticle contact in DEM

The kinetic and kinematic quantities related to an interparticle contact are illustrated in Fig. 1. In this study, the authors use a linear force–displacement model to calculate the normal force and the Coulomb frictional model for the tangential force with friction angle ϕ . The contact stiffnesses are determined from two material parameters E_c and ν_c by way of: $k_n = 2E_c r_1 r_2 / (r_1 + r_2)$ and $k_t = \nu_c k_n$, where r_1 and r_2 are the radii of the two contacting particles. Details of the solution procedure can be found in Guo & Zhao (2014).

RESULTS AND DISCUSSION

Test set-up

The domain of the TWHC test is of the same size as that of the experimental counterpart reported in Alsiny *et al.* (1992), with the cavity radius $r_c = 15$ mm and the outer radius $r_o = 150$ mm. The outer surface of the specimen is subjected to a constant confining pressure $\sigma_o = 100$ kPa. A uniform radial displacement u_c is applied to the inner surface of the specimen to inflate the cavity. Due to the axisymmetry, the cavity problem is often simulated with a quarter of the domain to save computational costs (e.g. Anand & Gu, 2000; Zervos *et al.*, 2001; François *et al.*, 2014; Desrues *et al.*, 2015). However, due to the grain-scale spatial heterogeneity of the RVEs, non-symmetric bifurcation mode may trigger and break the radial symmetry of the problem. Hence, the authors follow the approach in Papanastasiou & Vardoulakis (1992) and conduct quarter-domain and full-domain simulations, followed up with a further comparison of their results. The mesh and the boundary conditions for the simulations are illustrated in Fig. 2. For the quarter-domain mesh, 400 serendipity quadrilateral elements are used. The left and the bottom surfaces are subjected to roller boundary conditions. For the full-domain mesh, 1600 serendipity quadrilateral elements are used. Due to the axisymmetry, the hoop displacements of the four symmetric exterior nodes are restrained, as shown in Fig. 2 (Papanastasiou & Vardoulakis, 1992). Note that a reduced integration technique is used for all the simulations, which requires four Gauss quadrature points for each element (Zhao & Guo, 2015a).

In this study, the authors use 400 circular particles in the RVE packing with a roughly linear particle radius distribution from 3 to 7 mm. The choice of 400 particles is based on a sensitivity analysis detailed in Guo & Zhao (2014), and is a compromise between reliable RVE responses and affordable computational cost. Periodic boundary condition is enforced at both directions of the RVE. The particle density is set to 2650 kg/m^3 . The two contact stiffness

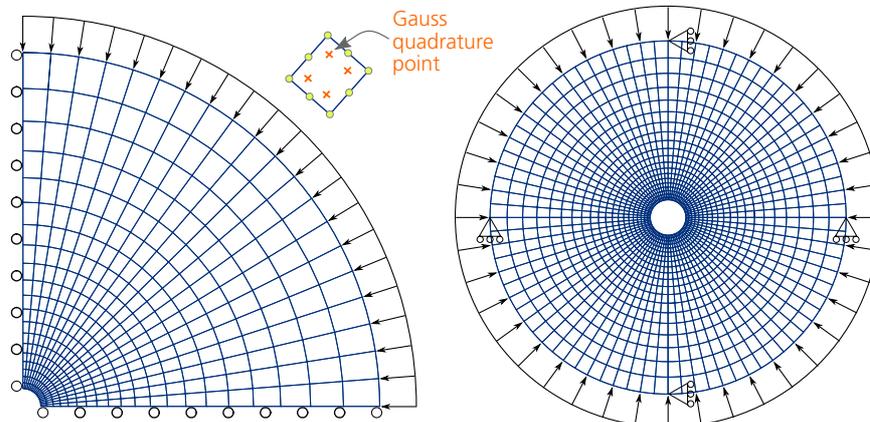


Fig. 2. Mesh and boundary conditions for quarter-domain and the full-domain simulations

parameters are $E_c = 600$ MPa and $\nu_c = 0.8$. The interparticle friction angle is $\phi = 0.5$. These material parameters are common in DEM modelling of sands and are consistent with those used in Guo & Zhao (2014). To reproduce qualitatively the typical responses of dense dry sand, the RVE packing is first isotropically consolidated to a mean effective stress $p_0 = \sigma_o = 100$ kPa and to reach a void ratio $e_0 = 0.177$. During the sample preparation process, the friction angle is reduced to achieve a relatively dense packing. After the preparation, the RVE packings – with the same initial conditions – are embedded into the Gauss quadrature points of the FEM mesh for the TWHC tests.

Cavity pressure

The authors first examine the evolution of the cavity pressure σ_c against the cavity expansion displacement u_c normalised by the initial cavity radius r_c , as plotted in Fig. 3. It is seen that the results from the simplified quarter-domain and the full-domain simulations are almost identical, despite some small deviations around the peak. Both show an obvious softening post-peak behaviour. From the drained biaxial compression test results on the same RVE packing (Guo & Zhao, 2014, 2015) shown in Fig. 4, the macroscopic material parameters, such as the peak friction angle ϕ_{\max} , the peak dilation angle ψ_{\max} and the elastic shear modulus G , can be estimated as: $\sin \phi_{\max} = ((\sigma_1/\sigma_3)_{\max} - 1)/((\sigma_1/\sigma_3)_{\max} + 1) \approx 0.47$, $\sin \psi_{\max} = ((d\varepsilon_1/d\varepsilon_3)_{\max} + 1)/(1 - (d\varepsilon_1/d\varepsilon_3)_{\max}) \approx 0.26$ (Bolton, 1986) and $G/p_0 \approx 113$, where σ_1 (ε_1) and σ_3 (ε_3) are the major and minor principal stresses (strains), respectively. With these estimations, it is instructive to further compare

the multiscale predictions with some closed-form solutions for the limit cavity pressure (Carter *et al.*, 1986; Yu & Houlsby, 1991). According to Yu & Houlsby (1991), the limit cavity pressure would reach about $15p_0$ (see Appendix) for the cohesionless sand based on an elasto-perfect-plastic constitutive model using the above estimated macroscopic material parameters. However, the current study gives a peak cavity pressure of only $3.5p_0$, as seen from Fig. 3, which is noticeably smaller than the analytical solution. The difference is mainly owing to the softening response of the material, as well as the highly non-uniform deformation field developed in the specimen due to strain localisation (other factors such as boundary condition and assumed two-dimensional simulation may also contribute). These two major factors violate the assumptions adopted in deriving the analytical solution. Indeed, from the experiments conducted by Alsiny *et al.* (1992) where strain localisation was observed, the cavity pressure can only reach up to a peak value slightly larger than $4p_0$ from different tests – with p_0 varying from 50 to 200 kPa – followed by a significant decreasing pressure, which are similar to the observations in this study. The complexities of the material response and the deformation field impede an accurate prediction of the limit cavity pressure based on simple assumptions, let alone a reliable prediction of the failure pattern. Therefore, a comprehensive numerical study on the failure mechanism and failure pattern is needed.

Strain localisation

Shear failure has been observed from both quarter-domain and full-domain simulations of the TWHC tests, where the failure pattern manifests as a series of curvilinear shear bands, as shown in Figs 5(a) and 5(b), in terms of the void ratio contours at two loading stages ($u_c = 7.5$ and 15 mm) (The entire development history of the shear bands can be found in the supplementary material of the paper.). For the quarter-domain simulation (Fig. 5(a)), a primary shear band is found emanating from the middle of the inner surface, propagating upwards along a spiral path, touching the left boundary and getting reflected before finally reaching the exterior surface (see the supplementary animation). The reflective boundary is artificially introduced by the imposed boundary condition that enforces axisymmetry in the quarter-domain modelling. This artificial effect is eliminated in the full-domain simulation (Fig. 5(b)) where four major antisymmetric shear bands have been observed, which are all initiated from the inner surface and develop uninterruptedly towards the exterior surface by following similar spiral patterns. A series of small curvilinear shear bands are also formed and these are intercepted by the primary shear bands. Figure 5(c) compares these two results with those

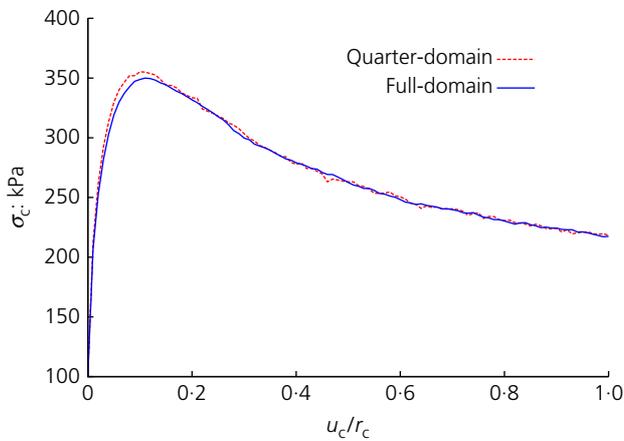


Fig. 3. Cavity pressure against normalised cavity expansion displacement

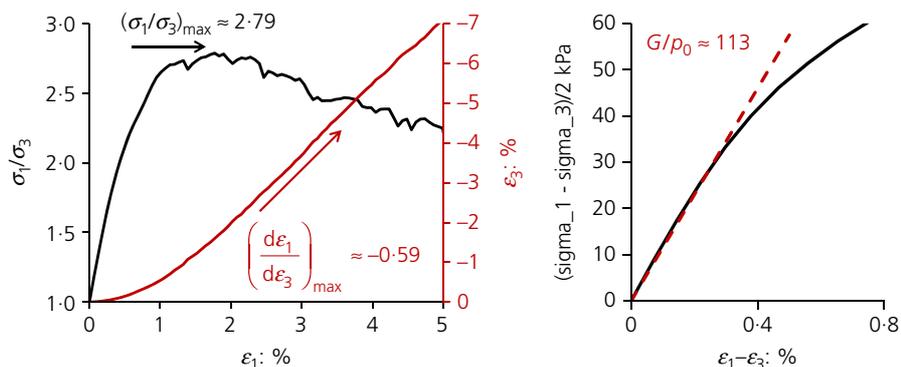


Fig. 4. Stress–strain relations and dilation from the drained biaxial compression test on the RVE

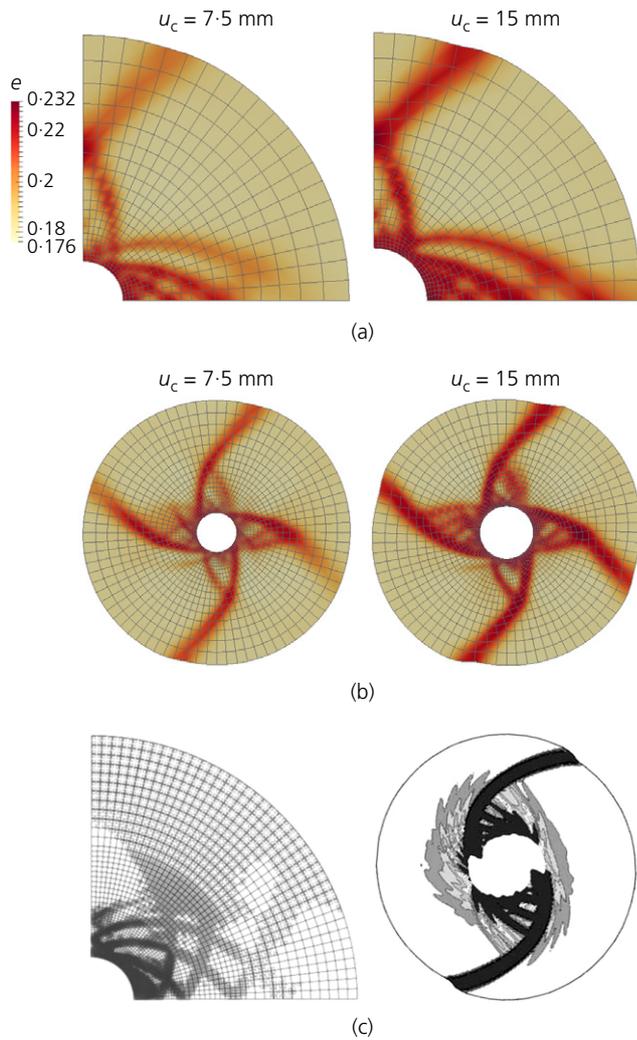


Fig. 5. Contours of void ratio at $u_c = 7.5$ and 15 mm showing strain localisation of (a) the quarter-domain and (b) the full-domain simulations; (c) comparison with other studies (figures adapted from François *et al.* (2014) and Crook *et al.* (2003), respectively)

from Crook *et al.* (2003) and François *et al.* (2014), which are obtained by way of macroscopic plasticity models. The authors' quarter-domain and full-domain simulations qualitatively agree well with the results obtained by using plasticity models.

Previous laboratory tests using digital image correlation and X-ray μ CT (Rechenmacher, 2006; Hall *et al.*, 2010) revealed that significant particle rotations take place inside the dilative shear band(s). This significant particle rotation is also observed in DEM simulations (Bardet & Proubet, 1991; Sun *et al.*, 2013a). In the multiscale model, the time history of the motion of each particle in the RVE packings is recorded. This unique aspect of the multiscale model enables us to measure the average particle rotation $\bar{\theta}$ of an RVE packing (averaged over all particles within the packing, positive for anti-clockwise rotation). Figure 6 shows the contours from the two tests at $u_c = 15$ mm. Clearly, particle rotations are concentrated at the localised dilative zones.

Microstructural analyses

The multiscale framework offers a convenient way for cross-scale analyses. Under the hood of macroscopic continuum modelling, the microstructure of the material points

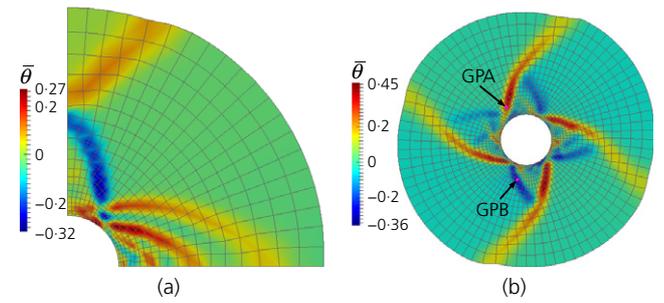


Fig. 6. Contours of average particle rotation at $u_c = 15$ mm of (a) the quarter-domain and (b) the full-domain simulations; GPA and GPB marked in (b) will be used for microstructural analyses

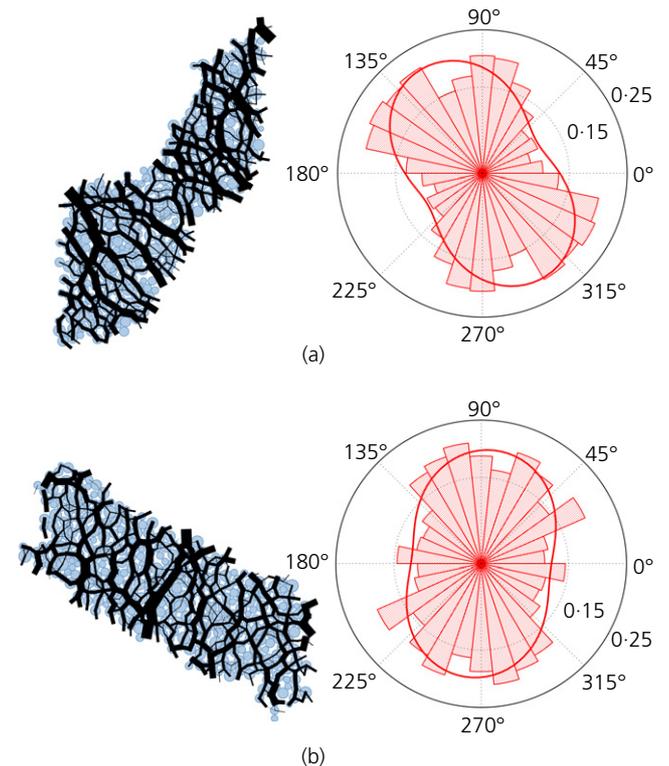


Fig. 7. Microstructures of local material points in terms of force chains and contact-normal distributions for (a) GPA and (b) GPB at $u_c = 15$ mm

can be characterised from the embedded RVE packings. Two such packings from different Gauss points of the full-domain simulation are chosen for demonstration. The two points – GPA and GPB – are located inside one of the primary (with positive $\bar{\theta}$) and one of the secondary (with negative $\bar{\theta}$) shear bands (Fig. 6(b)), respectively. Their microstructures after the cavity expansion at $u_c = 15$ mm (The entire evolution history of the force chains at these two points can be found from the animated video in the supplementary material of the paper.) are characterised by the force chains and the contact-normal distributions (or the so-called fabric tensor, Satake, 1982; Guo & Zhao, 2013; Zhao & Guo, 2013; Kuhn *et al.*, 2015), as shown in Fig. 7. First, it is seen that the RVE packings at both locations are severely stretched and rotated. The overall packing rotation of GPA is found to be anticlockwise, whereas that of GPB is clockwise, which are consistent with $\bar{\theta}$ at these two points. Second, distinct strong force chains (whose linewidth is proportional to the normal contact force) are observed

penetrating both packings, indicating that these two packings possess highly anisotropic structures. The major principal direction of the contacts can be seen from the rose diagram of the contact-normal distributions. At both locations, the major principal contact direction of the deformed RVE appears to be consistent with that of the strong force chains.

CONCLUSIONS

The authors have presented multiscale simulations of the TWHC tests in dry sand. Without the need of any macroscopic phenomenological model, the multiscale approach is capable of reproducing complex shear failure patterns manifested by a series of curvilinear shear bands observed in the TWHC experiments. The cavity pressure limit predicted by the multiscale model is noticeably smaller than its analytical counterpart, which is derived from a simple elasto-perfect-plastic model in the absence of shear banding. The multiscale approach is particularly suitable for macro-scale and microscale bridging. The microstructures of local material points and their evolutions under shearing can be conveniently examined. The simulation results indicate that significant particle rotation may develop inside shear bands and lead to highly anisotropic microstructures. One limitation of the study arises from the use of circular particles in the DEM model. For quantitative modelling of sand behaviours, realistic particle shape needs to be considered and this will be a future pursuit of the study.

APPENDIX

The simplified form of the cylindrical cavity pressure limit of a cohesionless elasto-perfect-plastic soil can be derived by assuming zero elastic strain within the plastic zone (Yu & Houlsby, 1991)

$$\frac{(\alpha + 1)\sigma_c}{2\alpha p_0} = \left[\frac{1}{1 - (1 - \delta)^{(\beta+1)/\beta}} \right]^{1/\gamma} \quad (3)$$

where the four material strength coefficients are defined as: $\alpha = (1 + \sin \phi'_{\max}) / (1 - \sin \phi'_{\max})$, $\beta = (1 + \sin \psi_{\max}) / (1 - \sin \psi_{\max})$, $\gamma = \alpha(\beta + 1) / [(\alpha - 1)\beta]$ and $\delta = (\alpha - 1)p_0 / [2(\alpha + 1)G]$. By substituting the estimated macroscopic strength parameters, these four coefficients are obtained as $\alpha \approx 2.77$, $\beta \approx 1.7$, $\gamma \approx 2.48$ and $\delta \approx 0.002$. Then the cavity pressure limit can be calculated from equation (3) as $\sigma_c \approx 15p_0$. This value is consistent with the range given in Figs 7–9 in Yu & Houlsby (1991).

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